University of Roma



RFID-Grids for Deformation Sensing

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Deformation of Structures

Processes in evolution involving structural deformations

- Civil infrastructures
- Cultural heritage
- Aircrafts/ships/vehicles

Multi-point information (map) required

- Control of a large surface
- Detection of unknown defects



Continuous Monitoring Network



Post-Disaster control



Disaster Prevention



Deformation of Structures Structural Health Monitoring (SHM)

A structure may Fail

- Aging
- Environment
- Accidental events
- · Design and manufacturing errors
- Unsatisfactory maintenance

SHM:

"The process of implementing monitoring strategies to give, at every moment during the life of a structure, a diagnosis of the "**state**" of the constituent **materials**, of the different **parts**, and of the full **assembly** of these parts constituting the structure as a whole."





Deformation of Structures In Numbers

Case	Typical Range	Resolution
Cracks in concrete Beams	1 mm	0.1mm
Cracks in steel reinforced concrete Beams	2-6 mm	0.5mm
Cracks in walls	2-4 mm	0.2mm
Cracks in tunnels' concrete slabs	0.1-0.2 mm	0.05mm
Deformation of foundations	1-10 mm	0.5mm
Cracks in Old and Historic buildings	1+ cm	1-2mm
Deformations in Ground Vibration Testing on Aerospace Structural Models	5cm	0.1mm

Tor vergata

Parametrization of Deformation

Stress

$$\bar{S} = lim_{A \to 0} \frac{F}{A}$$

 $\bar{d} = u(x, y, z)\hat{i} + v(x, y, z)\hat{j} + w(x, y, z)\hat{k}$

Therefore, a point P(x, y, z) will become, after the stress is applied, a new point P'(x + u, y + v, z + w).

	$arepsilon_x$	ε_{xy}	ε_{xz}
$\underline{\epsilon} =$	ε_{yx}	$arepsilon_y \ arepsilon_{zy}$	ε_{yz}
	ε_{zx}	ε_{zy}	ε_z
$arepsilon_x = 1$	$rac{ riangle dx}{dx} =$	$rac{\delta u}{\delta x}$	Normal strain

Strain



Constant Strain with Linear Displacement

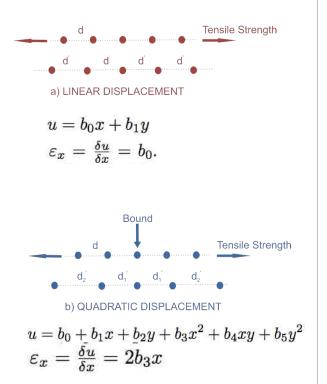
- All points subjected to the same constant strain.
- Equal-size segments are scaled in a same way during the deformation
- dilatation/compression of unbounded body,
- crack formation

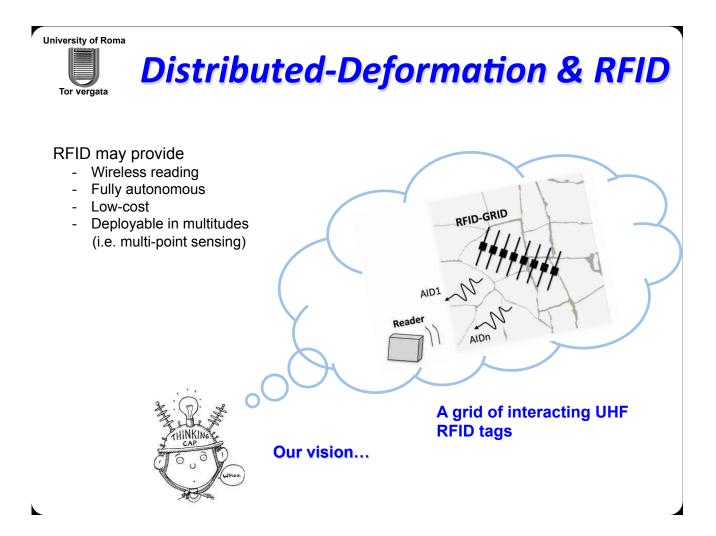
Linear Strain

with Quadratic Displacement

- Equal-size segments may be transformed in a different way depending on the position over the body
- deformation of bounded bodies,
- crack growth

Deformation Models







- Change of mutual distance between two antennas caused by deformation of the surface will produce a variation of the tag's response due to electromagnetic coupling
- Change of active impedance
- Change of embedded gain
- Deformation are remotely detectable by a RFID reader

Physical rationale engineering em. coupling

> 0.5 d/λ

→ RFID Grids

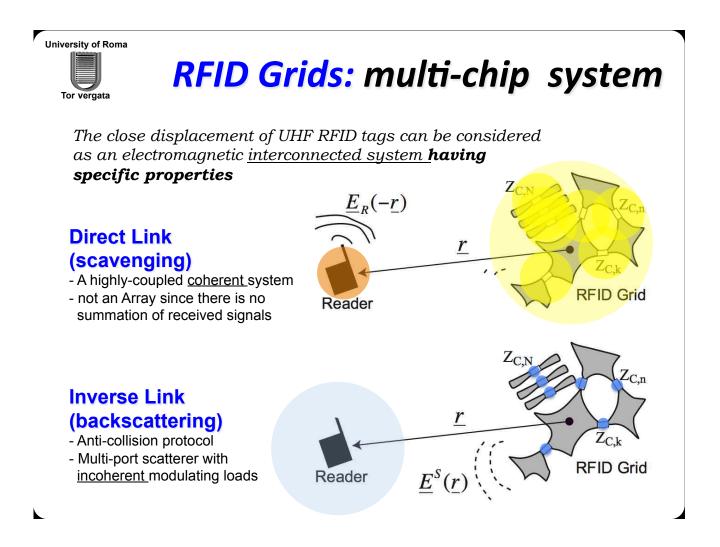
The idea may be extended to an array of tags

-40

0.1

0.2

0.3





Model: Multi-port scatterer

Radiation / scattering

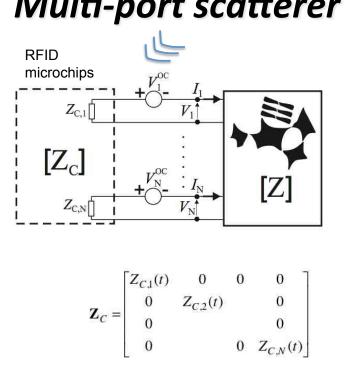
Embedded effective length & Gain

$$\left\{\underline{h}_{n}(\hat{\underline{r}}), G_{n}(\hat{\underline{r}})\right\}, n = 1.N$$

Impedances Network representation

$$\mathbf{I} = -\mathbf{Y}_G \cdot \mathbf{V}^{OC}$$

 $\mathbf{Y}_{G} = [\mathbf{Z} + \mathbf{Z}_{C}]^{-1} = [\mathbf{Z}_{G}]^{-1}$ Admittance Matrix of the Grid



G. Marrocco, "RFID GRIDS: Part I – Electromagnetic Theory", IEEE Trans. Antennas Propagat, March. 2011

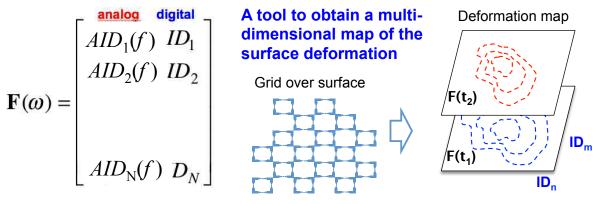
S. Caizzone, G. Marrocco, "RFID GRIDS: Part II - Experimentations", IEEE Trans. Antennas Propagat. Aug.2011





Analog IDentifier (AID) of Grid's elements $AID_n \equiv \frac{p_n}{2\sqrt{P_{R \leftarrow Tn}P_n^{to}}} = \alpha R_{C,n}|Y_{G,nn}|$ - Angle and position invariant - Environment invariant - Frequency dependent

RFID-GRID fingerprint



G. Marrocco, "**RFID GRIDS: Part I – Electromagnetic Theory**", *IEEE Trans. Antennas Propagat,* March. 2011 S. Caizzone, G. Marrocco, "**RFID GRIDS: Part II – Experimentations**", *IEEE Trans. Antennas Propagat.* Aug.2011



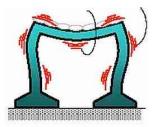
An Inverse Problem

The application of RFID-grid concept to the deformation observation requires the (measured) **variation of AID to be related to** (unknown) change of **inter-element spacing or distributed strain**



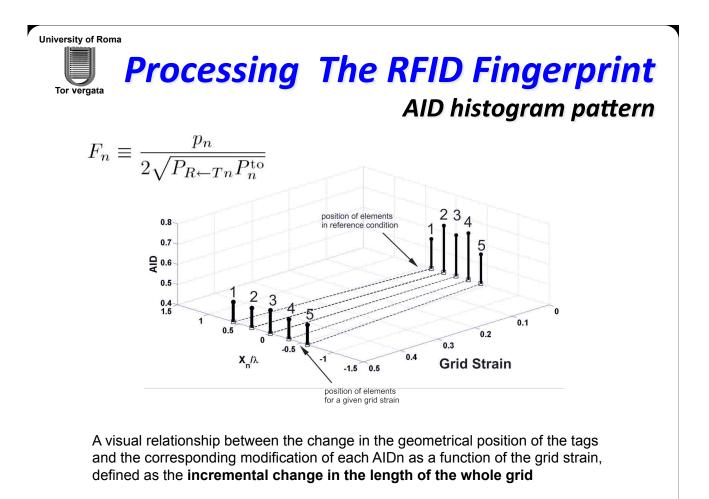
Cracks ←→ displacement

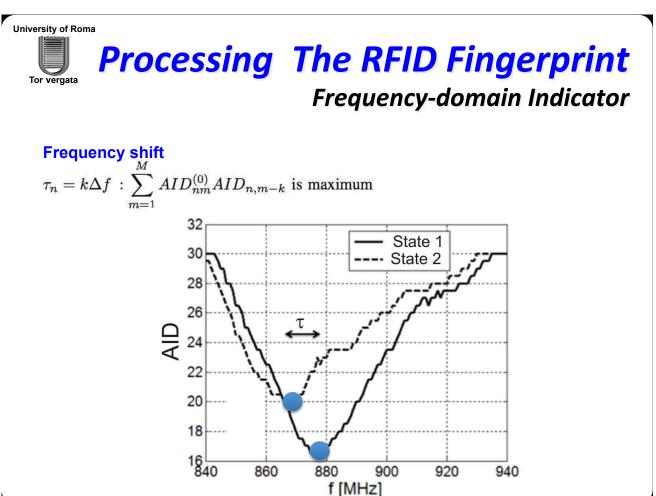
$$d \Leftarrow f[F(\omega)]$$



Structural deformations ←→ strain

 $\varepsilon \Leftarrow f[\boldsymbol{F}(\boldsymbol{\omega})]$









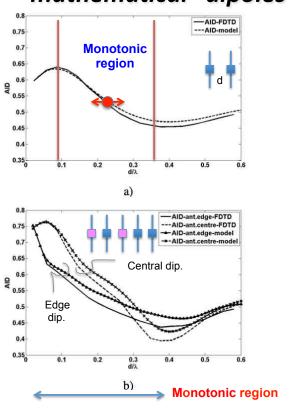
- Theoretical formulas for mutual impedance of side-by-side dipoles
- Self impedance of standalone configuration

$$Z = \begin{bmatrix} Z_s & Z_{12}(d_{12}) & Z_{13}(d_{13}) & \dots & Z_{1n}(d_{1n}) \\ Z_{21}(d_{21}) & Z_s & Z_{23}(d_{23}) & \dots & Z_{2n}(d_{2n}) \\ \dots & \dots & \dots & \dots & \dots \\ Z_{m1}(d_{m1}) & Z_{m2}(d_{m2}) & Z_{m3}(d_{m3}) & \dots & Z_s \end{bmatrix}$$

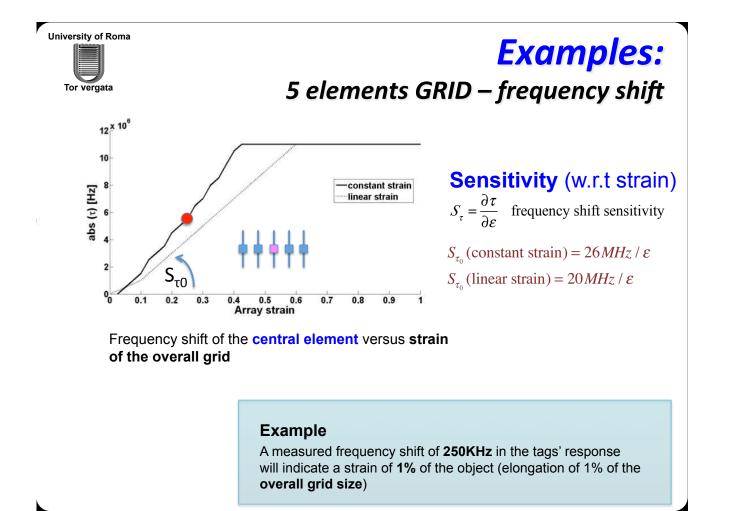
$$Z_{mn} = \frac{\eta}{2\pi} (-2E_i(ju_0) + E_i(ju_1) + E_i(ju_2))$$

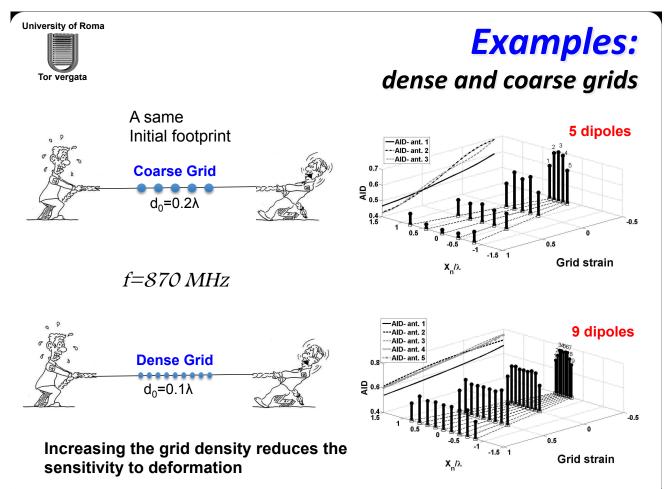
 E_i : Exponential function

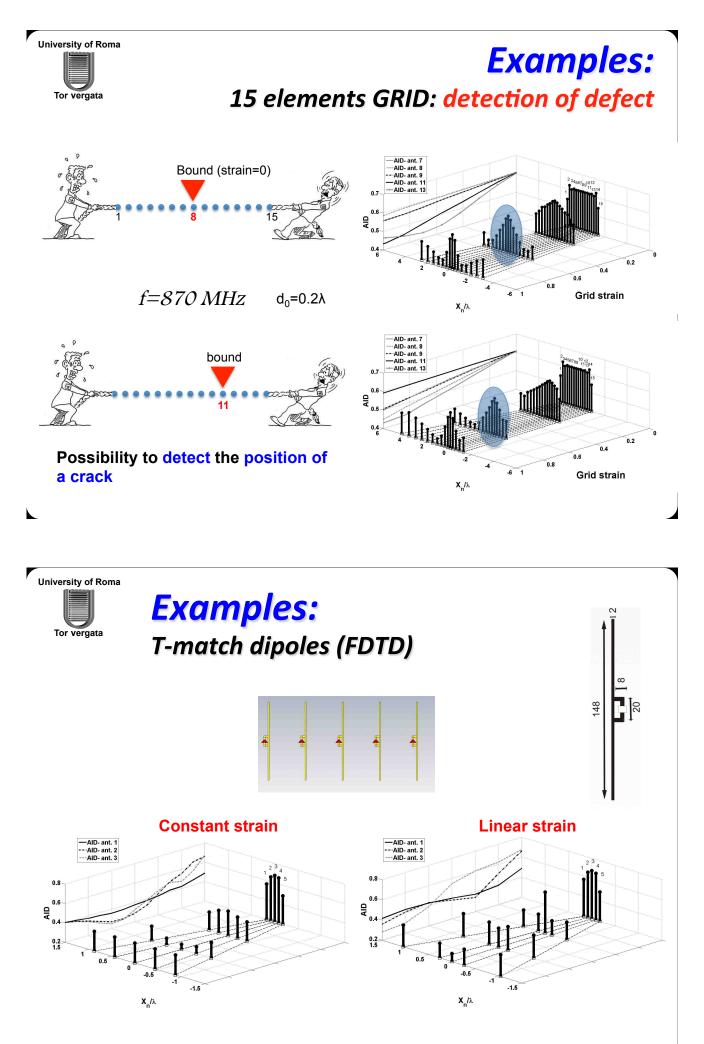
$$AID_n = R_{C,n} \left| Y_{G,nn} \right|$$



University of Roma **Examples:** 5-elements GRID ("mathematical" dipoles) Tor vergata -AID- ant. 1 •AID- ant. 2 d₀=0.2λ AID- ant. 3 0.7 ₽^{0.6} Tractive Tractive force force 0.4 -0.5 **Constant strain** 0.5 -1.5 Grid strain **Χ**_/λ f=870 MHz -AID- ant. 1 AID- ant. 2 AID- ant. 3 Spatial constraint 0.7 입^{0.6} Tractive Tractive force force 0.4 1.5 0.5 0.5 0 **Linear strain** 1 -0.5 1.5 Grid strain -1.5 2 X_n/λ



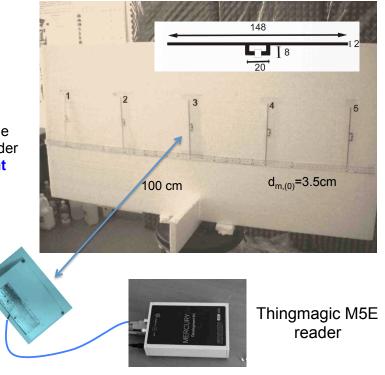






Experiment Five T-match dipoles

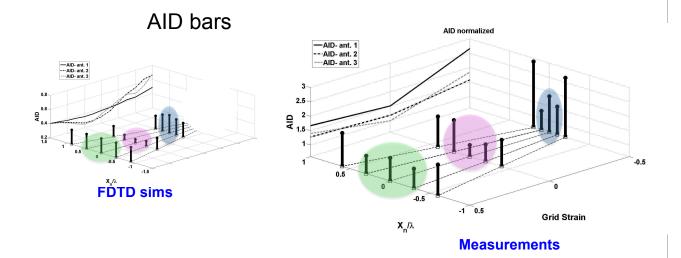
- The grid lays over a foam-like substrate.
- ThingMagic M5E reader + broad band PIFA antenna in broadside orientation at distance, L=100cm
- The positions of the tags inside the grid **are manually changed** in order to simulate **a linear displacement** (compression and elongation).
- Initial condition (zero strain)
- inter-tag distance d_m=3.5cm (0.2λ at 870MHz).



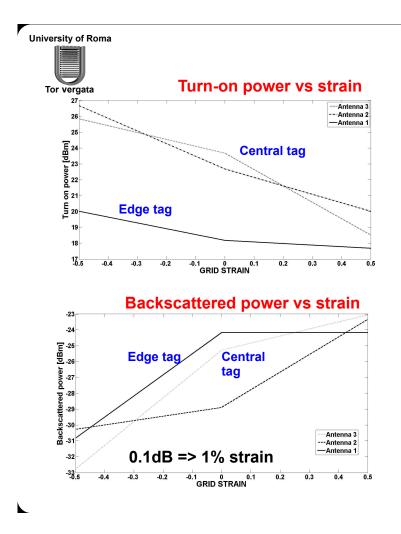


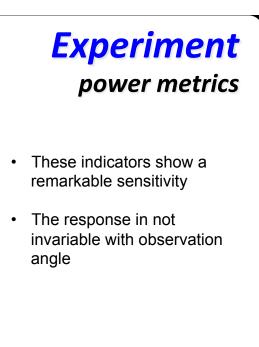


Experiment Five T-match dipoles



Edge elements behaves differently than simulations since FDTD model does not account for the non-linearity of microchip impedances





Sensitivity-Central tag $S(backscatt) = 9.7 dB / \varepsilon$ $S(turn - on) = 7.3 dB / \varepsilon$



Discussion Sensing vs. reader's resolution

Example:

N=5 d₀=5.5cm (initial inter-antenna distance) Strain: constant

Achieved GRID Sensitivity

$\Delta p_{BS,\min} \leq S_{BS} \cdot \varepsilon_{\min}$ $\Delta p_{BS,\min} \leq S_{BS} \cdot \frac{\Delta d}{d_0}$	Desired system resolution	AID S _τ =25MHz/ε	Backscattering S _{BS} =10dB/ε
	Δd_{min}=0.1mm Aerospace Structures, cracks in concrete	Reader resolution: ∆f _{min} < 40kHz	Reader resolution Δp_{min} < 0.015 dB
cracks	Δd_{min}=1mm cracks in historical buildings	∆f _{min} < 400 kHz	Δp _{min} < 0.15dB
deformations	ε _{min} = 0.1%	Reader resolution: ∆f _{min} < 25 kHz	Reader resolution Δp _{min} < 0.01dB
	ε _{min} =1%	∆f _{min} < 250kHz	Δp _{min} <0.1dB





- RFID grids' fingerprint might be a promising tool to
 - estimate the **overall amount** of surface deformation
 - o provide a local representation of the displacement
 - o identify defects
- Other indicators, such as **turn-on power or backscattered power, can provide bigger variation levels**, but need fixed setups
- **Grid-spacing controls the sensitivity** (coarse grids are better, provided that tags' response lay in the monotonic region)
- The Grid sensitivity may be improved by investigate **more-coupled lattices** (physically interconnected system)
- **Phase-change** may be also considered thanks to new readers
- Sensing-oriented readers (Δp<=0.1dB) and ad-hoc processing tools are required to form a true imaging system